

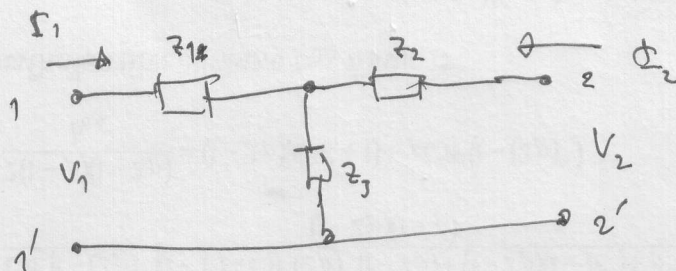
Transmission Line

(1)

1000 JAMU M0 2/2054

vs (1)

in Z, Y parameters



in Z - parameters

$$V_1 = Z_{11}I_1 + Z_{12}I_2 \quad (1)$$

$$V_2 = Z_{22}I_2 + Z_{21}I_1 \quad (2)$$

in $Z_{11} \rightarrow$ open $V_2 \rightarrow I_2 = 0$ (open on $2-2'$)

$$Z_{11} = Z_1 + Z_3$$

in $Z_{12} \rightarrow$ open $V_1 \rightarrow I_1 = 0$

$$Z_{12} = \frac{V_1}{I_2} \Big|_{I_1 = 0}$$

open V_1

$$V_1 = I_2 Z_3$$

$$\therefore Z_{12} = \frac{I_2 Z_3}{I_2} = Z_3$$

in $Z_{21} \rightarrow$ open $V_2 \rightarrow I_2 = 0$

$$Z_{21} = \frac{V_2}{I_1} \Big|_{I_2 = 0}$$

open V_2

$$V_2 = I_1 Z_3$$

$$\therefore z_{21} = \frac{\cancel{\Phi_1} z_3}{\cancel{\Phi_1}} = z_3 \quad \longrightarrow$$

in $z_{22} \Rightarrow$ open $V_2 \rightarrow \Phi_1 = 0$

$$z_{22} = \frac{V_2}{\Phi_2} \quad \left| \quad \Phi_1 = 0 \right.$$

$$V_2 = \Phi_2 z_2 + \Phi_2 z_3 = \Phi_2 (z_2 + z_3)$$

$$z_{12} = \frac{\Phi_2 (z_2 + z_3)}{\Phi_2} = z_2 + z_3 \quad \longrightarrow$$

$$[Z] = \begin{bmatrix} z_{11} & z_{12} \\ z_{21} & z_{22} \end{bmatrix} = \begin{bmatrix} z_1 + z_3 & z_3 \\ z_3 & z_2 + z_3 \end{bmatrix}$$

in $[Y]$ parameter

$$[Y] = [Z]^{-1} \quad \rightarrow \text{invert } [Z]$$

in $[Z]^{-1} \rightarrow$

$[Adjoint Z] =$

\oplus $z_1 + z_3$	\ominus z_3
\ominus z_3	\oplus $z_2 + z_3$

 \rightarrow

$+(z_2 + z_3)$	$- z_3$
$- z_3$	$+ z_1 + z_2$

$$\Delta^1 [Z] = (z_1 + z_3)(z_2 + z_3) - z_3^2 = z_1 z_2 + z_1 z_3 + z_3 z_2 + \cancel{z_3^2} - \cancel{z_3^2}$$

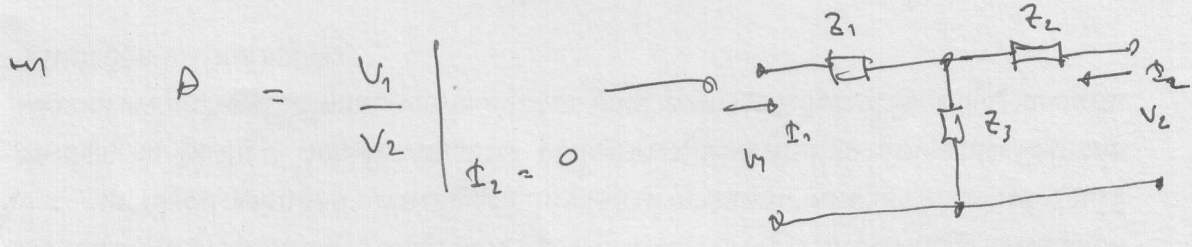
$$|z| = z_1 z_2 + z_1 z_3 + z_3 z_2$$

$$[Y] = [z]^{-1} = \begin{bmatrix} \frac{z_2 + z_3}{z_1 z_2 + z_1 z_3 + z_3 z_2} & \frac{-z_3}{z_1 z_2 + z_1 z_3 + z_3 z_2} \\ \frac{-z_3}{z_1 z_2 + z_1 z_3 + z_3 z_2} & \frac{z_1 + z_2}{z_1 z_2 + z_1 z_3 + z_3 z_2} \end{bmatrix}$$

in [F] parameter.

$$V_1 = A V_2 - B \Phi_2$$

$$\Phi_1 = C V_2 - D \Phi_2$$



open V_2

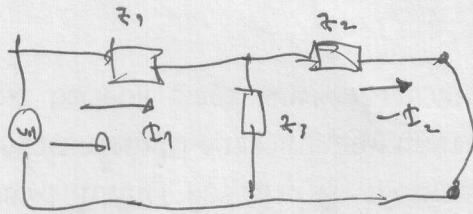
$$V_2 = \frac{V_1 \times z_3}{z_1 + z_3} = \frac{V_1 z_3}{z_1 + z_3}$$

in $A = \frac{V_1}{\frac{V_1 z_3}{z_1 + z_3}} = \frac{z_1 + z_2}{z_3}$

$$A = \frac{z_1 + z_2}{z_3}$$

in $B = \frac{V_1}{-\Phi_2} \Big|_{V_2 = 0}$ short

if $V_2 \rightarrow$ short



$$z_T = z_1 + z_2 // z_3 = z_1 + \frac{z_2 z_3}{z_2 + z_3}$$

$$z_T = \frac{z_1(z_2 + z_3) + z_2 z_3}{z_2 + z_3}$$

$$I_1 = \frac{V_1}{z_T} = \frac{V_1}{\left[\frac{z_1 z_2 + z_1 z_3 + z_2 z_3}{z_2 + z_3} \right]}$$

$$I_1 = V_1 \left[\frac{z_2 + z_3}{z_1 z_2 + z_1 z_3 + z_2 z_3} \right]$$

if $I_2 \rightarrow$ find the value of V_2 .

$$-I_2 = \frac{I_1 z_3}{z_2 + z_3}$$

if I_1 is given

$$-I_2 = \frac{V_1 (z_2 + z_3)}{z_1 z_2 + z_1 z_3 + z_2 z_3} \times \frac{z_3}{(z_2 + z_3)}$$

$$-I_2 = \frac{V_1 z_3}{z_1 z_2 + z_1 z_3 + z_2 z_3}$$

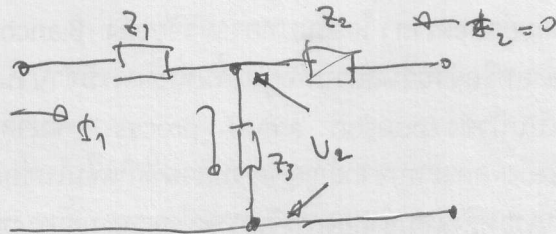
if

$$B = \frac{V_1}{-I_2} \Big|_{V_2=0} = \frac{V_1}{\left[\frac{V_1 z_3}{z_1 z_2 + z_1 z_3 + z_2 z_3} \right]}$$

$$\beta = \frac{z_1 z_2 + z_1 z_3 + z_2 z_3}{z_3}$$

in c case

$$c = \frac{\phi_1}{V_2} \Big|_{\phi_2 = 0} \quad (\text{open } V_2)$$

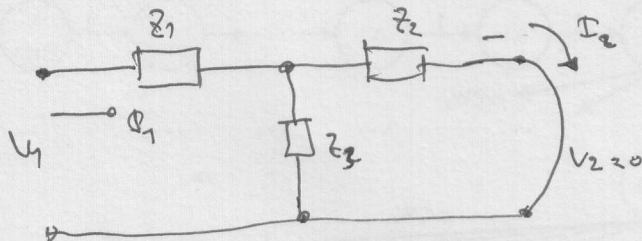


$$V_2 = \phi_1 z_3$$

$$\therefore c = \frac{\phi_1}{\phi_1 z_3} = \frac{1}{z_3}$$

in d case

$$d = \frac{\phi_1}{-\phi_2} \Big|_{V_2 = 0} \quad \rightarrow \text{short } V_2$$



total flux \$V_1 \Rightarrow z_T = z_1 + (z_2 || z_3)\$
 flux divider rule.

$$-\phi_2 = \frac{\phi_1 z_3}{z_2 + z_3}$$

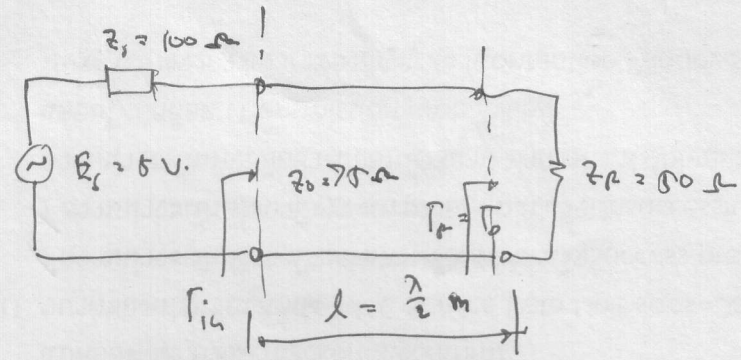
$$d = \frac{\phi_1}{\left[\frac{\phi_1 z_3}{z_2 + z_3} \right]} = \frac{z_2 + z_3}{z_3}$$

$$[F] = \begin{bmatrix} A & B \\ C & D \end{bmatrix}$$

$$[F] = \begin{bmatrix} \frac{z_1 + z_3}{z_3} & \frac{z_1 z_2 + z_1 z_3 + z_2 z_3}{z_3} \\ \frac{1}{z_3} & \frac{z_2 + z_3}{z_3} \end{bmatrix}$$

2

Don P_{in} , P_L , P_R , $P_{L,R}$ von ~~den~~ Z_1, Z_2, Z_0



$$\Gamma_{in} = \frac{Z_0 - Z_{in}}{Z_0 + Z_{in}} = \Gamma_0 e^{-j\beta l}$$

$\Gamma_0 = \frac{Z_R - Z_0}{Z_R + Z_0}$

$\frac{1}{8}$

oder 2×10^{-2}

$$P_{in} = \frac{1}{8} \frac{|E_s|^2 |1 - \Gamma_0|^2}{|1 - \Gamma_0 \Gamma_0 e^{-2j\beta l}|^2} (1 - |\Gamma_0 e^{-2j\beta l}|^2)$$

$$\Gamma_0 = \frac{Z_R - Z_0}{Z_R + Z_0} = \frac{50 - 75}{50 + 75} = 0.1428$$

$$\Gamma_0 = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{75 - 50}{75 + 50} = -0.2$$

$$\beta = \frac{2\pi}{\lambda}$$

$$\beta l = \frac{2\pi}{\lambda} \times \frac{\lambda}{2} = \pi$$

$$r e^{j\theta} = r \cos \theta + j r \sin \theta = r (\cos \theta + j \sin \theta)$$

$$e^{-2j\beta l} = e^{-2j(\pi)} = e^{j(-2\pi)} = \cos(-2\pi) + j \sin(-2\pi)$$

$$e^{-2j\beta l} = 1 + (0) = 1$$

Return Γ_{in} 0.1429

$$P_{in} = \frac{1}{8} \frac{|E_s|^2 |1 - \Gamma_s|^2}{|1 - \Gamma_s \Gamma_0|^2} |1 - \Gamma_0|^2$$

$$P_{in} = \frac{1}{8} \frac{5^2 (1 - 0.1429)^2}{[1 - (0.1429)(-0.2)]^2} [1 - (-0.2)]^2$$

$$P_{in} = \frac{1}{8} \frac{18.369}{1.05749} (1.2)^2 = 3.125 \text{ W}$$

$$P_L = P_{in} = 10 \log \frac{3.125 \text{ W}}{1 \text{ W}} = 4.948 \text{ dB} \quad \text{--- } \square$$

$$\text{Return loss} = (RL) = \cancel{10 \log \frac{1}{1.4}} - 10 \log (|\Gamma_{in}|)^2$$

$$\Gamma_{in} = \Gamma_0 e^{-j\beta l} = 0.2 (-0.2) e^{-j(0)}$$

$$\Gamma_{in} = (-0.2) [\cos(-360) + j \sin(-360)]$$

$$\Gamma_{in} = (-0.2)(+1 + 0) = -0.2$$

$$\text{Return loss} = 10 \log (0.2^2) = \cancel{10} + 13.975 \text{ dB}$$

$$\text{Insertion loss} = (IL) = 10 \log (1 - |\Gamma_{in}|^2)$$

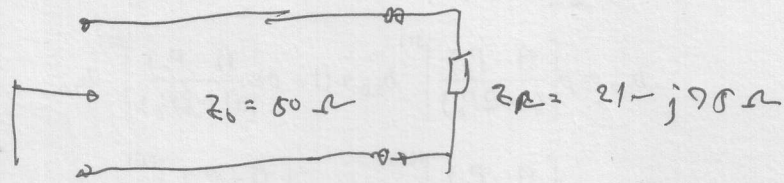
$$= 10 \log (1 - (0.2)^2) = 10 \log 0.56$$

Insertion loss = -0.19928 dB \rightarrow

(3)

3

to find SWR and reflection coefficient



P_{in} = 10W

$$Z_r \text{ (normalized)} = \frac{21 - j75}{50} = 0.42 - j1.5$$

Reflection Coefficient

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{21 - j75 - 50}{21 - j75 + 50}$$

$$\Gamma = \frac{-29 - j75}{71 - j75} = \frac{80.41 \angle -111.13^\circ}{103.27 \angle -46.56^\circ}$$

$$\Gamma = 0.7786 \angle -64.57^\circ$$

$$|\Gamma| = 0.7786 \text{ --- } \text{Mag: } 0.7786$$

$$SWR = \frac{1 + |\Gamma|}{1 - |\Gamma|} = \frac{1 + 0.7786}{1 - 0.7786}$$

$$SWR = 8.03342 \text{ --- } \text{Mag: } 8.03342$$

Smith chart

$$\eta = \frac{\text{กำลังใช้ไป}}{\text{กำลังงานที่จ่ายให้หลอด}} = \frac{1}{1.4}$$

$$\text{กำลังงานที่จ่ายให้หลอด} = \eta \times \text{กำลังใช้ไป}$$

$$= 0.4 \times 10 \text{ W}$$

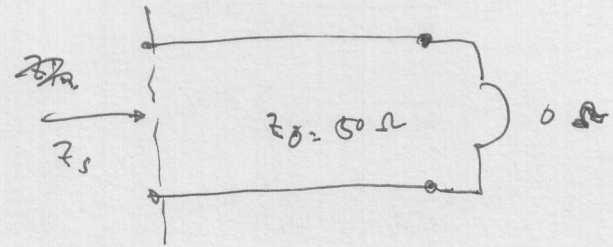
$$= 4 \text{ watt} \quad \text{---} \oplus$$

④ $\Gamma_{in} = 0.305$ $\Gamma_{out} = 0.305$ $\Gamma_{in} = \Gamma_{out}$

$$l = 0.305 \lambda_p \quad \left| \quad f = 4 \text{ GHz} \right.$$

กรณี ① short circuit $\rightarrow Z_L = 0 \Omega$

เมื่อ load เป็น short



$$Z_s = j Z_0 \tan \beta l$$

$$\beta l = \frac{2\pi}{\lambda_p} (0.305) \lambda_p$$

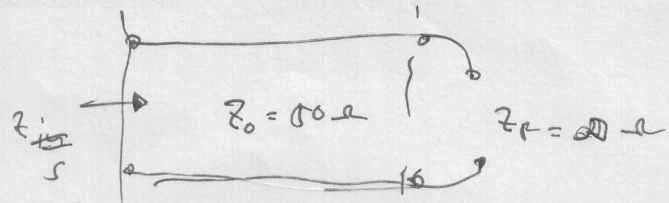
$$\beta l = 109.8$$

$$Z_s = j (50) \tan 109.8$$

$$Z_s = -j 178.88 \Omega$$

$$Z_s (\text{normalized}) = \frac{-j 178.88}{50} = -j 3.577 \Omega$$

กรณี ② open circuit $\rightarrow Z_L = \infty \Omega$



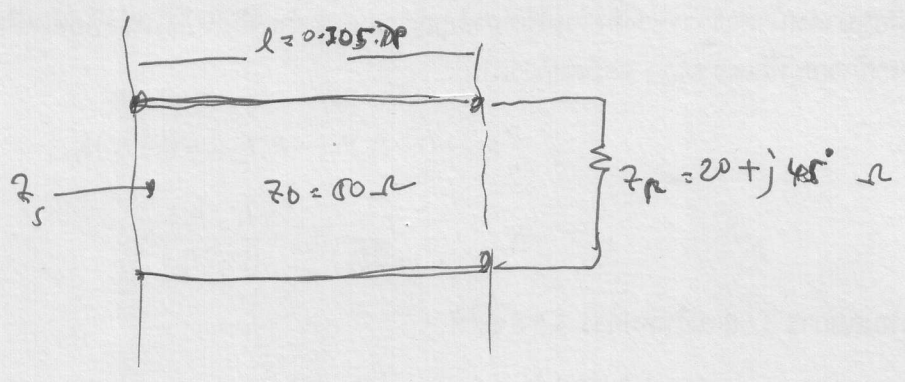
now simplify

$$Z_s = \frac{-jZ_0}{\tan \beta l} = \frac{-j50}{\tan \frac{2\pi}{\lambda} (0.305\lambda)}$$

$$Z_s = \frac{-j50}{-2.777} = +j18.0 \Omega$$

$$Z_{in} \text{ normalized} = j \frac{18}{50} = +j0.360 \Omega$$

now ③ $Z_0 = 50 \Omega$ $Z_L = 20 + j45 \Omega$



$$Z_s = \frac{Z_0 (Z_L + j Z_0 \tan \beta l)}{Z_0 + j Z_L \tan \beta l}$$

$$Z_s = \frac{50 (20 + j45 + j50 \left[\tan \frac{2\pi}{\lambda} (0.305\lambda) \right])}{50 + j(20 + j45) \tan \frac{2\pi}{\lambda} (0.305\lambda)}$$

$$Z_s = \frac{1000 + j2250 - j6944.01}{50 + j20 + j^2 45 (-2.777)}$$

$$Z_s = \frac{1000 - j4694.01}{174.96 + j20} = \frac{4799.7 \angle -97.9}{176.09 \angle 6.52}$$

$$Z_s = 27.25 \angle -84.42$$

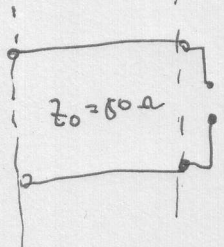
$$Z_s = 2.649 - j27.12 \quad \Omega$$

$$Z_s \text{ (normalized)} = \frac{Z_s}{Z_0} = \frac{2.649 - j27.12}{50}$$

$$Z_s' = 0.0529 - j0.5424 \quad \text{--- } \Omega$$

96 s with chord

near $Z_0 = 2$ (open circuit)



The Complete Smith Chart

Black Magic Design

$$Z'_s = \frac{Z_L}{Z_0} = \frac{2}{50} = 0.04$$

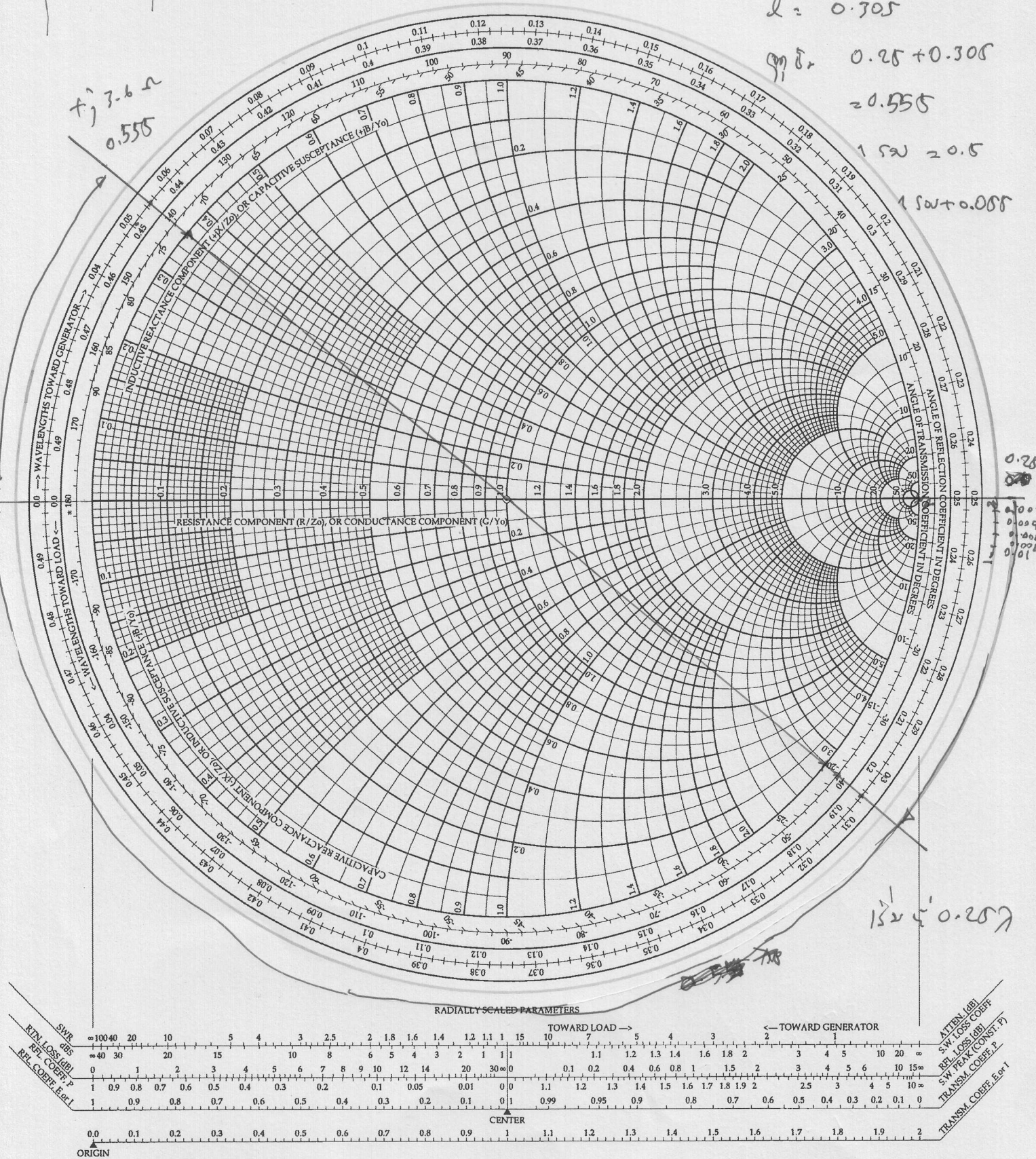
$$Z'_s = 2 + j2 \Omega$$

$$l = 0.305$$

$$0.25 + 0.305 = 0.555$$

$$1.52 = 0.5$$

$$1.52 + 0.085$$



$f_j 3.6 \Omega$
 0.555

0.25
100
100
100
100
100

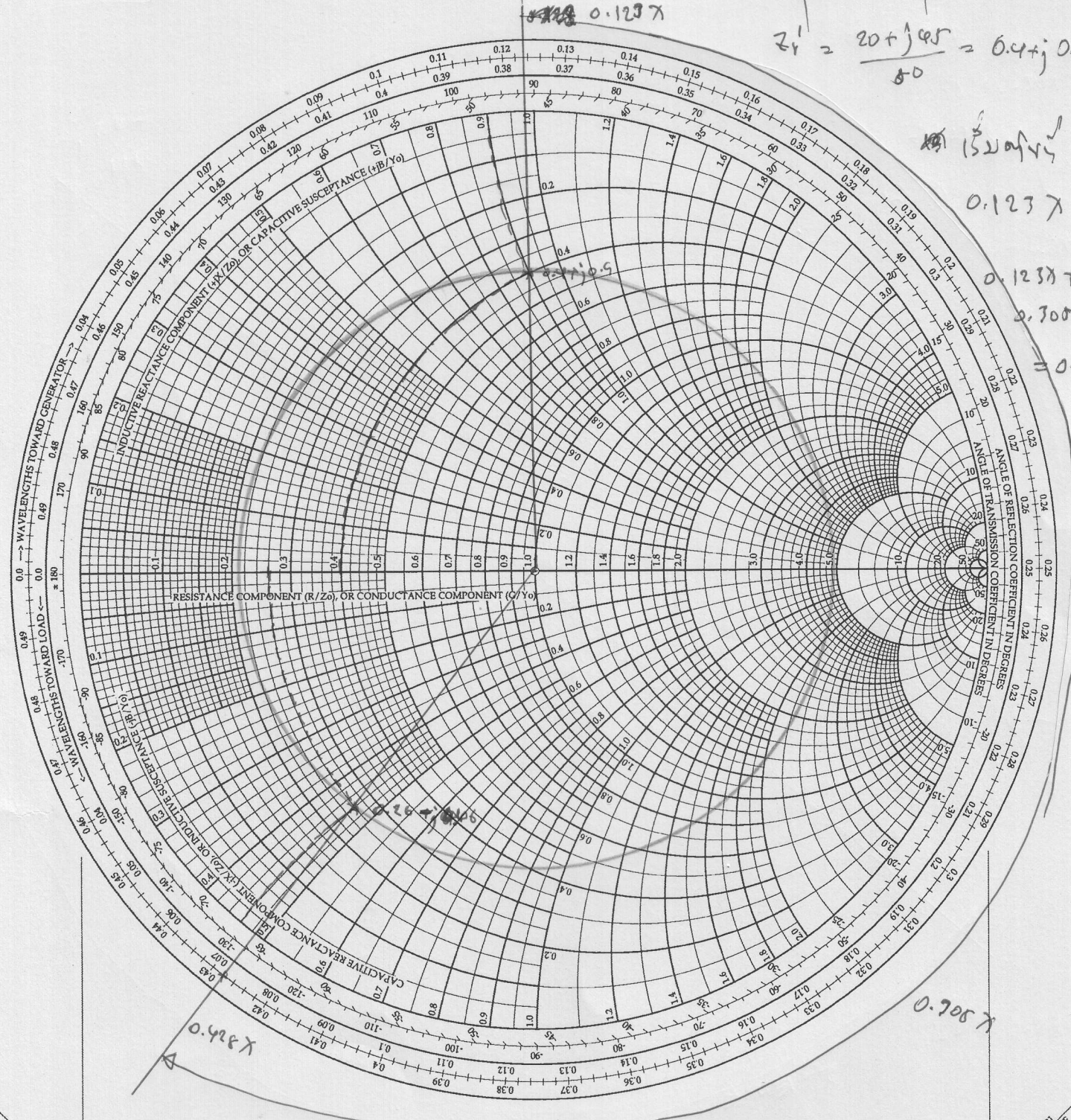
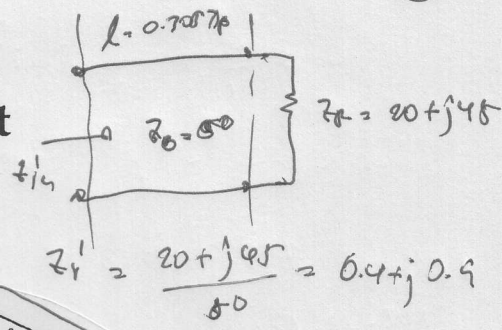
0.25
 0.25

smith chart
 $Z_{in} = +j0.36$
 $Z_{in} = +j0.36 \Omega$

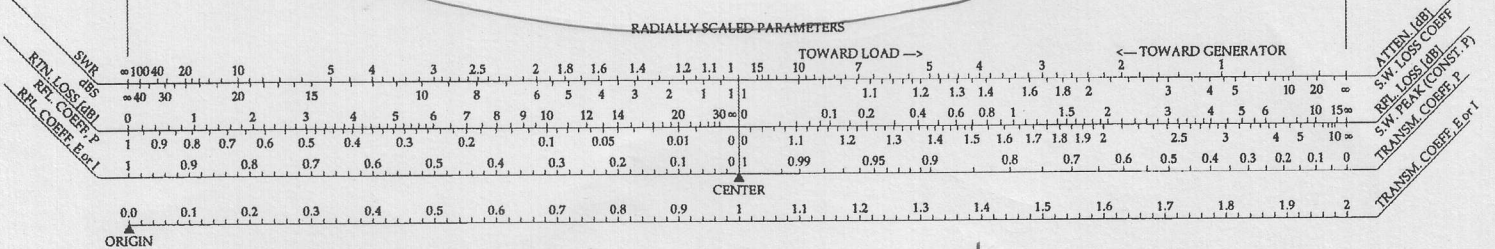
$Z_L = 20 + j45$

The Complete Smith Chart

Black Magic Design



0.123 λ
 0.123 λ +
 0.705 λ
 = 0.428 λ

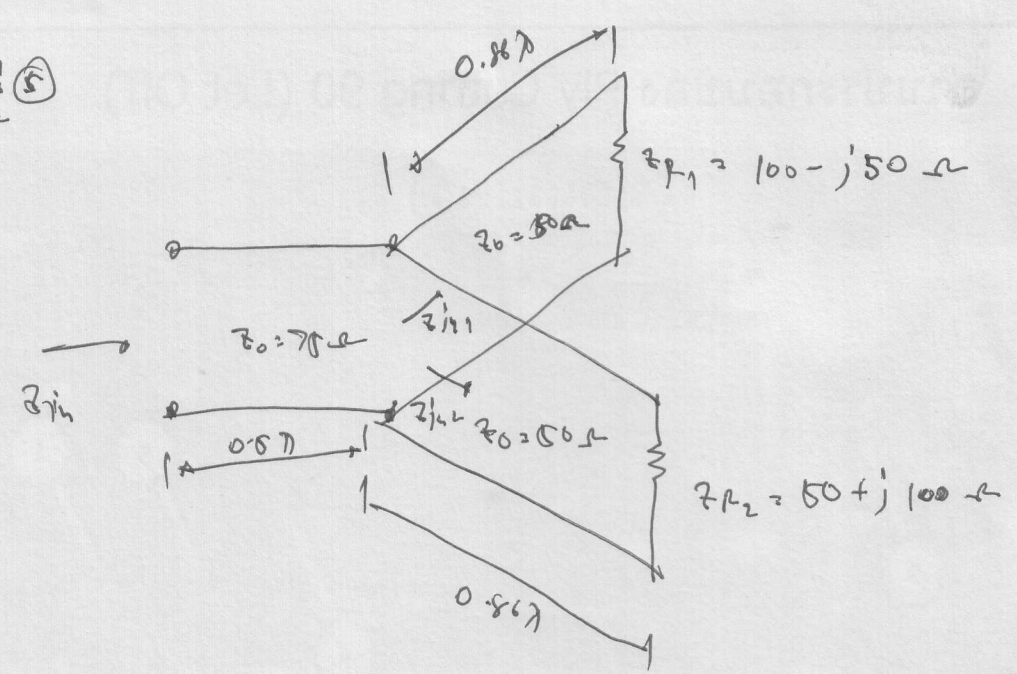


$Z_T = 0.26 - j0.46$

$Z_s = 26 - j46 \Omega$

$Z_s = (0.26 - j0.46) \times 50 = 13 - j23 \Omega$

21 (5)



Assume Z_0

$$Z_{in1} = \frac{Z_0 (Z_L + j Z_0 \tan \beta l)}{Z_0 + j Z_L \tan \beta l}$$

or $\frac{Z_L}{Z_0}$ given in V.R. 85 v

$$Z_{in1} = \frac{Z_0 \left(\frac{Z_L}{Z_0} + j \tan \beta l \right)}{1 + \frac{Z_L}{Z_0} \tan \beta l}$$

$$\frac{Z_L}{Z_0} = \frac{100 - j50}{50} = 2 - j1$$

$$\tan \beta l = \tan \frac{2\pi}{\lambda} (0.8\lambda) = \tan (2\pi \times 0.8)$$

$$\tan \beta l = -1.208$$

$$Z_{in1} = \frac{50 [2 - j + j (-1.208)]}{1 + (2 - j) (-1.208)}$$

$$Z_{in1} = \frac{100 - j50 - j1.208}{1 + 2 - j(-1.208)}$$

$$Z_{in1} = \frac{100 - j81.208}{3 + j1.208} = \frac{112.348 \angle -29.11}{3.234 \angle +21.93}$$

$$Z_{in1} = 34.73 \angle -49.04 \ \Omega$$

$$Y_{in1} = \frac{1}{Z_{in1}} = \frac{1}{34.73 \angle -49.04} = 0.02879 \angle 49.04 \ \text{S}$$

$$Y_{in1} = 0.01889 + j0.02194 \ \text{S}$$

$$Z_{in2} = \frac{Z_0 \left(\frac{Z_L}{Z_0} + j \tan \beta l \right)}{1 + \frac{Z_L}{Z_0} \tan \beta l}$$

$$\frac{Z_L}{Z_0} = \frac{50 + j100}{50} = 1 + j2$$

$$\tan \beta l = \tan \frac{Z_L}{Z_0} (0.56\lambda) = \tan 309.5^\circ = -1.2087$$

$$Z_{in2} = \frac{50 \left[(1 + j2) + j(-1.2087) \right]}{1 + (1 + j2)(-1.2087)} = \frac{50 + j100 - j60.435}{1 - 1.2087 - j2.4174}$$

$$= \frac{50 + j39.565}{-0.2087 - j2.4174} = \frac{50 + j39.6}{-0.2087 - j2.416}$$

$$= \frac{63.78 \angle 38.39}{2.424 \angle -94.92}$$

$$= 26.311 \angle 137.25 = -18.04 + j19.151$$

$$Y_{in2} = \frac{1}{26.311 \angle 137.29} = 0.038 \angle -137.29$$

$$Y_{in2} = 0.038 \angle -137.29 = -0.026 - j0.0276$$

$$Y_{in3} = Y_{in1} + Y_{in2} = 0.01889 + j0.02174 - 0.026 - j0.0276$$

$$Y_{in3} = -0.00713 - j0.00586$$

$$Y_{in3} = 0.009225 \angle -140.58^\circ$$

$$Z_{in3} = \frac{1}{Y_{in3}} = \frac{1}{0.009225 \angle -140.58} = 108.354 \angle 140.58^\circ \Omega$$

$$Z_R = Z_{in3}$$

$$Z_{in} = \frac{Z_0 \left(\frac{Z_R}{Z_0} + j \tan \beta l \right)}{1 + \frac{Z_R}{Z_0} \tan \beta l}$$

$$\frac{Z_R}{Z_0} = \frac{108.354 \angle 140.58^\circ}{75}$$

$$\frac{Z_R}{Z_0} = 1.444 \angle 140.58^\circ$$

$$\tan \beta l = \tan \frac{2\pi}{\lambda} (0.5\lambda) = \tan 180^\circ = 0$$

$$-Z_{in} = \frac{75 (1.444 (140.58 + j'0))}{7 + (1.444 (140.58 (0)))}$$

$$Z_{in} = 108.3 (140.58) \quad \Omega$$

$$Z_{in} = -83.663 + j 68.77$$

$$Z_{in}' = \frac{Z_{in}}{Z_0} = \frac{Z_{in}}{75} = -1.1158 + j 0.916 \quad \Omega$$

(normalized)

Equivalent circuit

Step 1 ① $\frac{Z_1}{Z_0} = \frac{100 - j50}{50} = 2 - j1 = Z_1'$

Step 2 ② ~~the~~ matching Z_2' is required.

$$Y_{in} = \frac{1}{Z_1'} = \frac{1}{2 - j1} = 1.3 - j1.18 \quad S$$

Step 3 ③ when $Z_{in2} = 50 + j100$

$$Z_{in2}' = \frac{50 + j100}{50} = 1 + j2$$

Step 4 ④ when $Z_{in2}' \rightarrow$ is required $\Delta \Gamma$

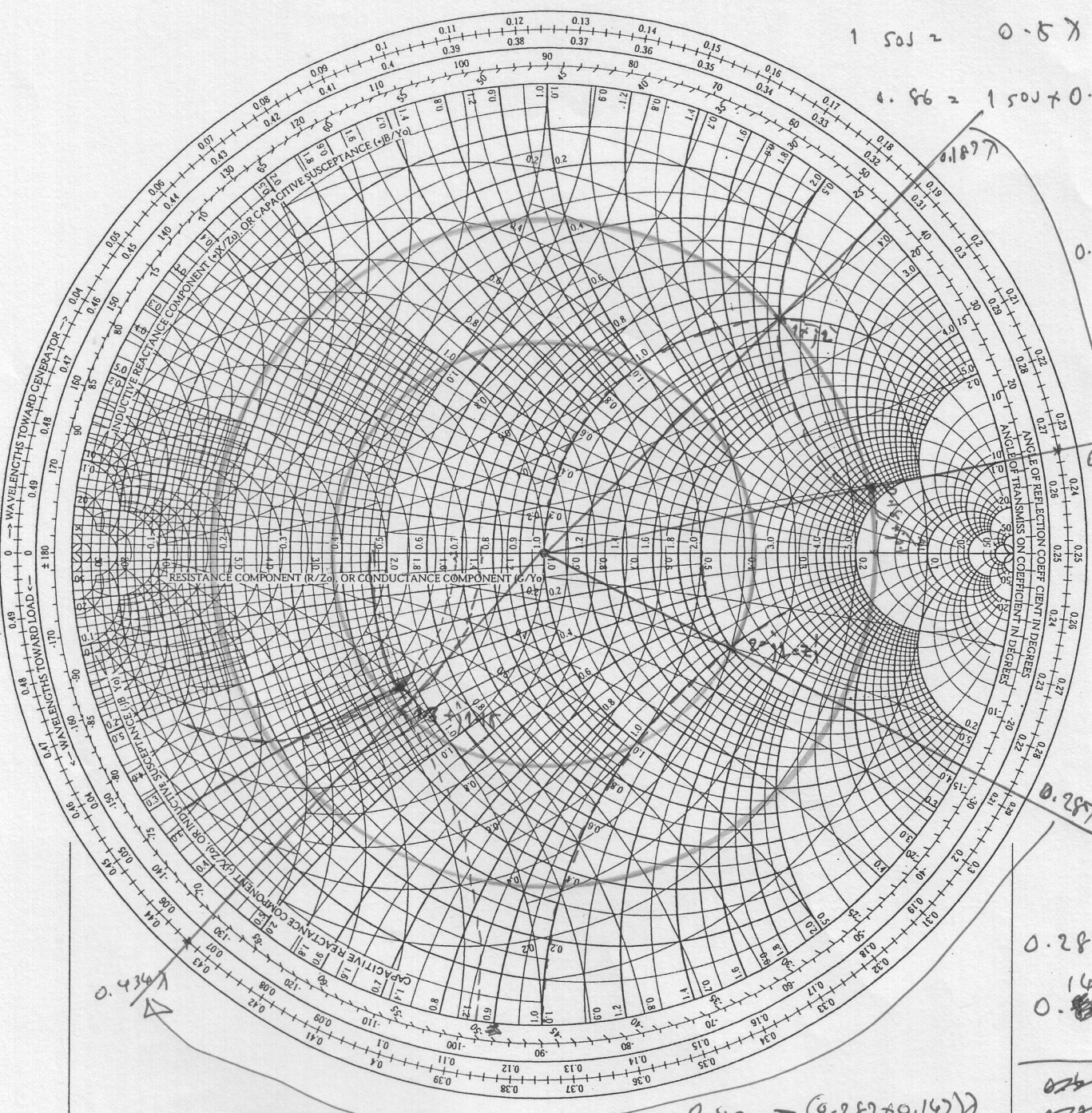
NAME	TITLE	DWG. NO.
SMITH CHART	Courtesy of Microwaves101.com	DATE

NORMALIZED IMPEDANCE AND ADMITTANCE COORDINATES

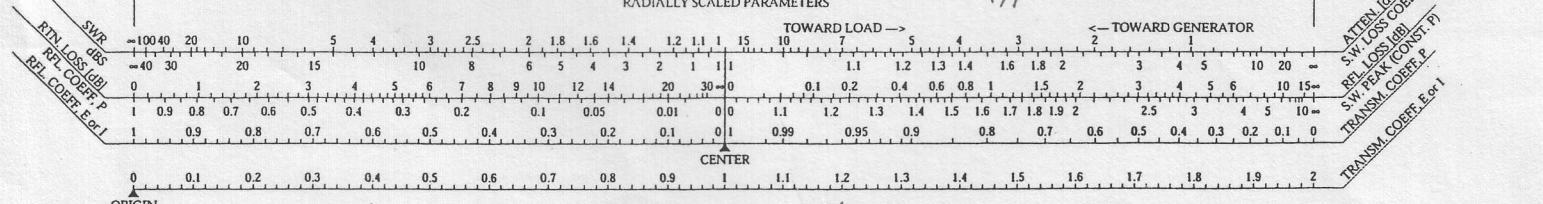
0.86λ

1.50λ = 0.5λ

0.86 = 1.50λ + 0.36λ



RADIALLY SCALED PARAMETERS



$Z_{in} = 0 + j100$

$Z_{in} = Z_{in} = \frac{0 + j100}{5} = 1 + j2$

$1.3 \rightarrow 0.189\lambda + 0.86\lambda$
 $= 1.049\lambda = 2.50\lambda + 0.049\lambda$
 $= 0.189\lambda + 0.049\lambda = 0.234\lambda$

$1.149 = 2.50\lambda + 0.149$

$Y_{in} = 1.3 + j1.15$

~~0.289λ~~
~~0.16λ~~
~~0.434λ~~
~~0.974λ~~

$$I_2 - Y_{in2} = 0.18 + j0.1 \text{ S}$$

$$Y_{in3} = Y_{in1} + Y_{in2} = 1.3 - j1.18 + (0.18 + j0.1)$$

$$Y_{in3} = 1.48 - j1.08 \text{ S}$$

Step ② මගින් Y_{in3} → එහි පරිපූරක සමස්ත ප්‍රතිරෝධය.

$$Z_{in3}' = 0.48 - j0.32 \text{ } \Omega$$

$$Z_{in3} (\text{JMS}) = Z_{in3}' \times 50 = (0.48 - j0.32) 50$$

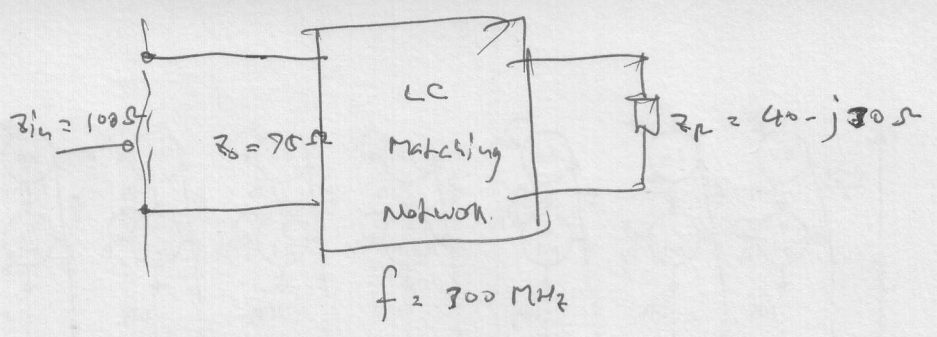
$$Z_{in3} (\text{JMS}) = 24 - j16 \text{ } \Omega$$

Z_{in3} → පරිපූරක (සමස්ත) පරිපූරක පරිපූරක ~~විද්‍ය~~ $Z_0 = 75 \text{ } \Omega$

එහි පරිපූරකය $\frac{Z}{2}$ → $Z_{in} = Z_{in3}$

$$Z_{in} = 24 - j16 \text{ } \Omega$$

6



soln

$$Z_L' = \frac{Z_L}{Z_0} = \frac{40 - j30}{75}$$

$$Z_L' = 0.5333 - j0.4$$

$$Z_{in}' = \frac{Z_{in}}{Z_0} = \frac{100}{75} = 1.333 + j0$$

or Z_L' and Z_{in}' → solve with eqn.

for Z_L' → we use Z_{in}' → find the series reactance inductance.

find L or series reactance

$$Z_A = 0.5333 + j0.5$$

$$jX_L = Z_A - Z_L' = 0.5333 + j0.5 - (0.5333 - j0.4)$$

$$jX_L = 0.5333 + j0.5 - 0.5333 + j0.4$$

$$jX_L = j0.9$$

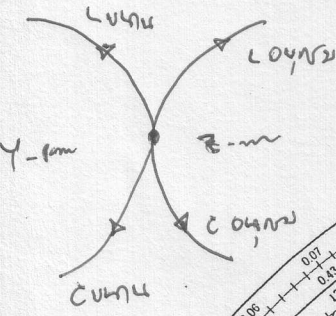
$$X_L = 0.9$$

$$X_L(\text{ohms}) = 0.9 \times Z_0 = 0.9 \times 75$$

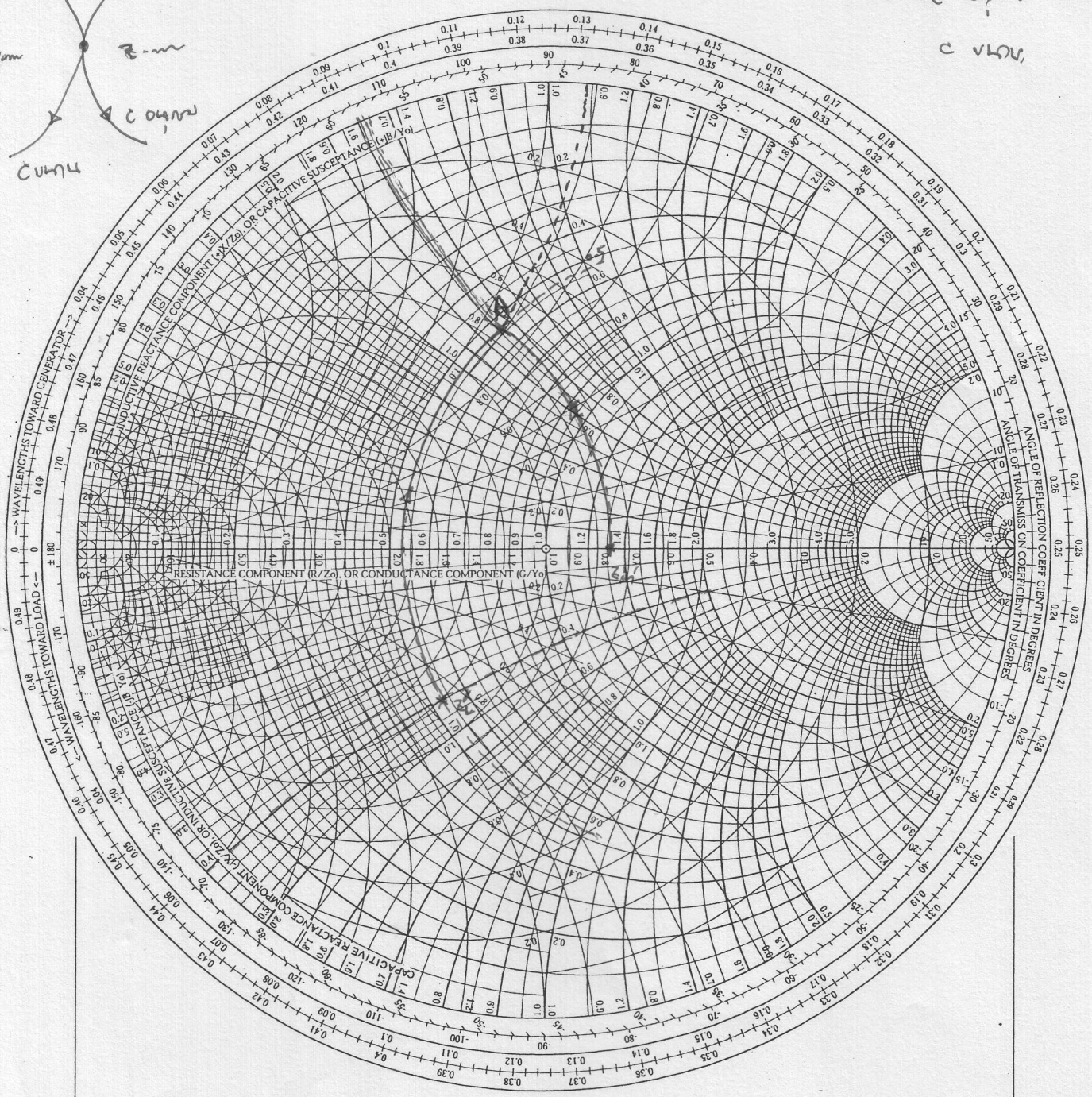
$$X_L(\text{ohms}) = 67.5 \text{ } \Omega$$

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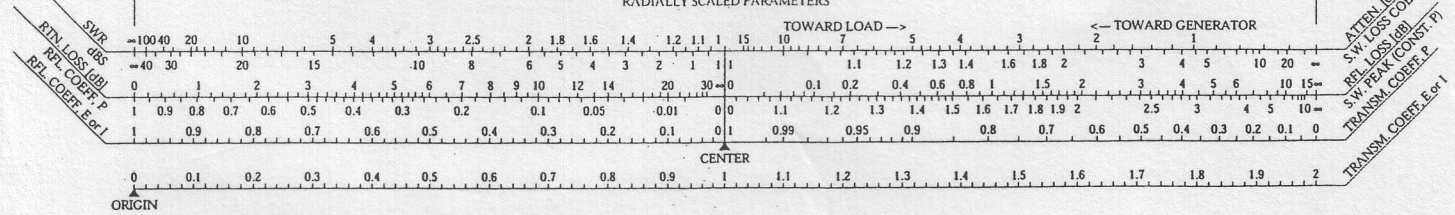
NORMALIZED IMPEDANCE AND ADMITTANCE COORDINATES



L 04λ/8
C 04λ/8



RADIALLY SCALED PARAMETERS



$Z_L = 0.5333 - j0.4 \quad \Omega$
 $Z_{in} = 2.333 + j0 \quad \Omega$

$$2\pi fL = 67.5$$

$$L = \frac{67.5}{2\pi \times 300 \times 10^6}$$

$$L = 0.0358 \mu\text{H} \rightarrow 35.8 \text{ nH}$$

$$Y_A = 0.75 + j0.93$$

$$Y_{in} = 0.95 + j0$$

$$j b_c = Y_{in} - Y_A = 0.95 - (0.75 + j0.93)$$

$$j b_c = 0.95 - 0.75 - j0.93$$

$$j b_c = -j0.93$$

$$b_c = 0.93$$

$$2\pi fC = 0.93$$

$$b_c \omega_0 = 0.93 \times \omega_0 = 0.93 \times \frac{1}{95}$$

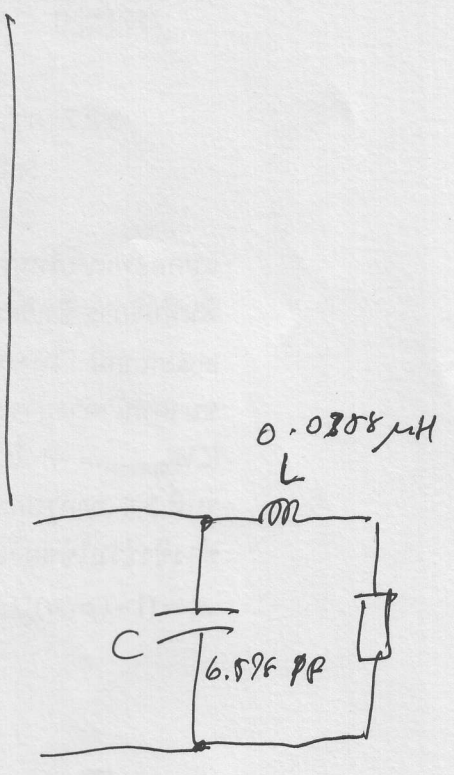
$$= 0.93 \times \frac{1}{95}$$

$$b_c = 0.0124$$

$$2\pi fC = 0.0124$$

$$C = \frac{0.0124}{2\pi \times 300 \times 10^6} = 6.598 \times 10^{-12} \text{ F}$$

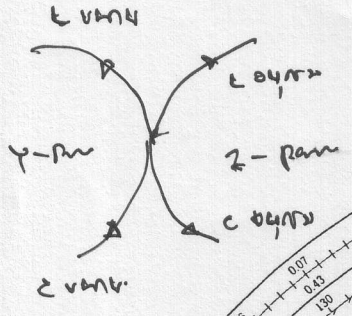
$$C = 6.598 \text{ pF}$$



vs rary

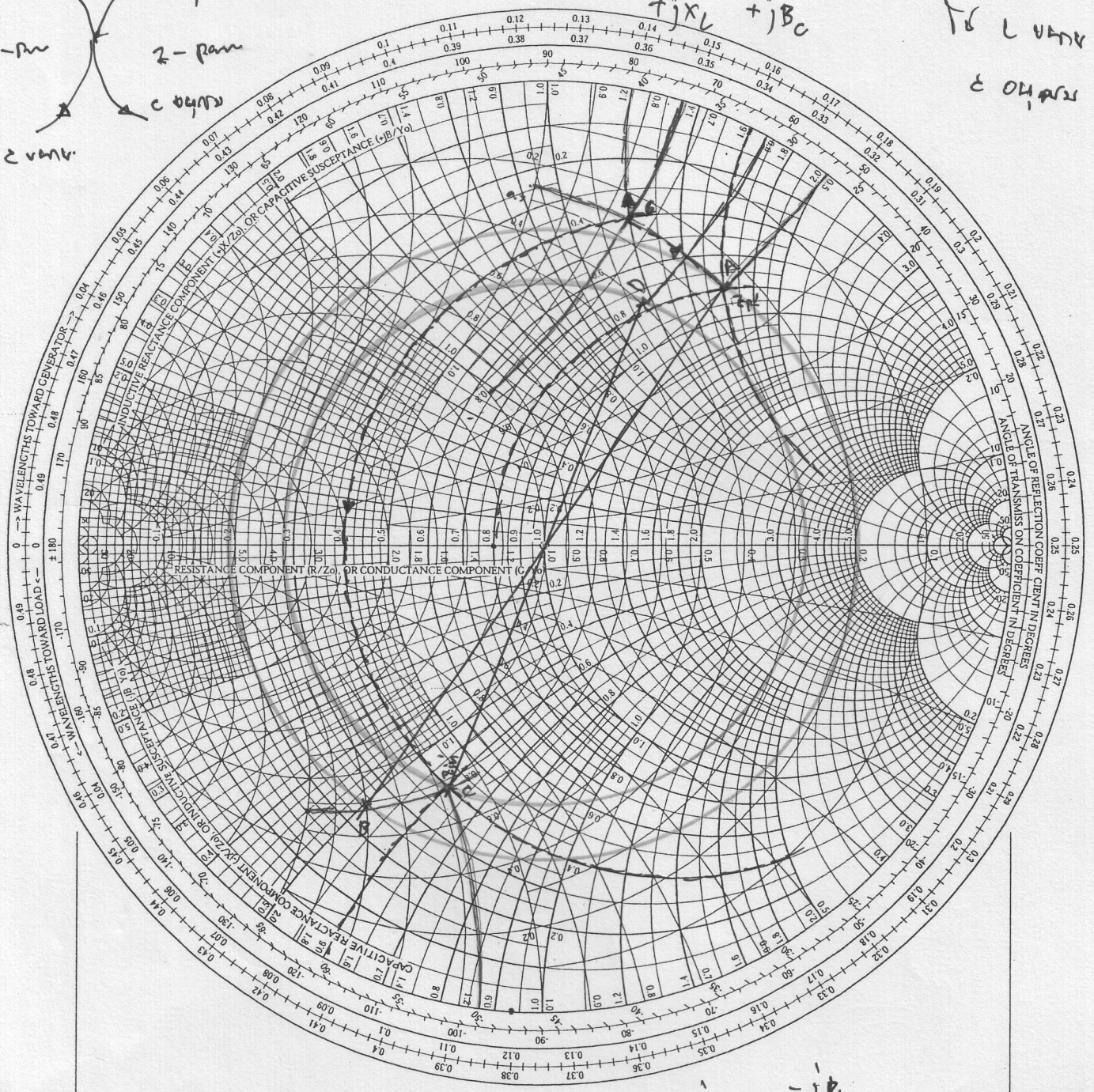
NAME	TITLE	DWG. NO.
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NORMALIZED IMPEDANCE AND ADMITTANCE COORDINATES

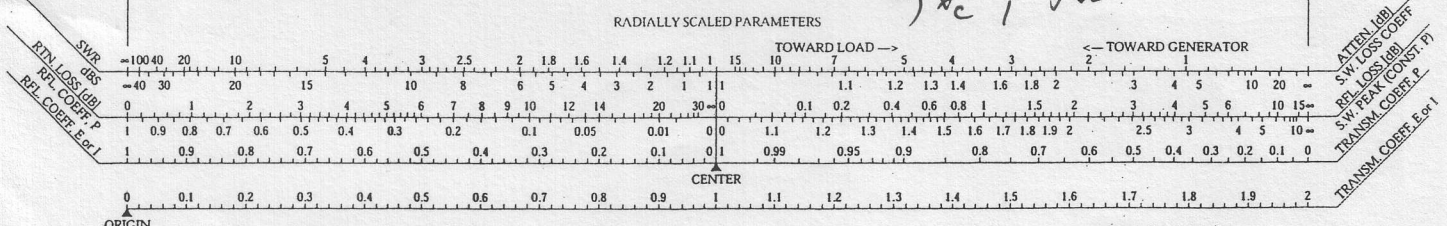


$tjXL + jBc$

$Tb L jXL$
 $C - jXC$



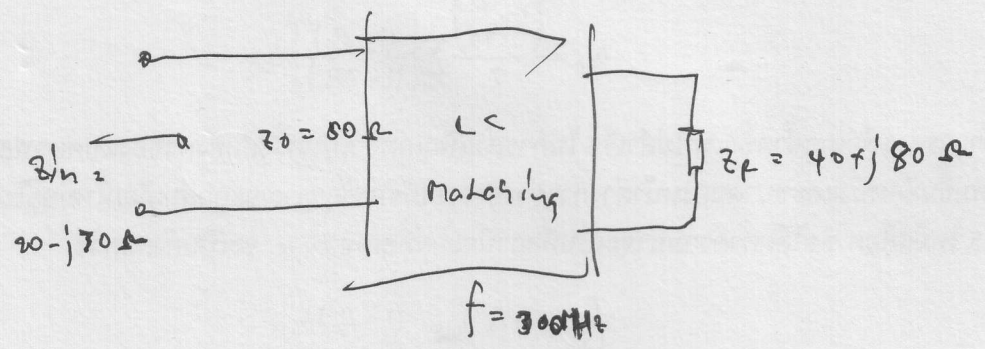
$-jxc, -jBc$



$z_1 \rightarrow z$
 $D \rightarrow y$
 $A \rightarrow z$
 $B \rightarrow y$

$\} \text{ scale } 1/n \text{ scale} \rightarrow z$
 $\} \text{ scale } 1/n \text{ scale} \rightarrow z$

48 (7)



soln

$$Z'_L = \frac{Z_L}{Z_0} = \frac{Z_L}{80} = \frac{40 + j80}{80} = 0.5 + j1.0$$

1) Plot Z'_L on smith chart. Point A
 and determine A for

$$Y'_L = 0.25 - j0.5 \quad S$$

$$Z'_L = 0.5 + j1.0 \quad \Omega$$

2) $Z'_{in} = \frac{Z_{in}}{Z_0} = \frac{20 - j30}{80} = 0.25 - j0.375$

Plot Z'_{in} on smith chart point B and determine B.

$$Y'_{in} = 0.75 + j1.125 \quad S$$

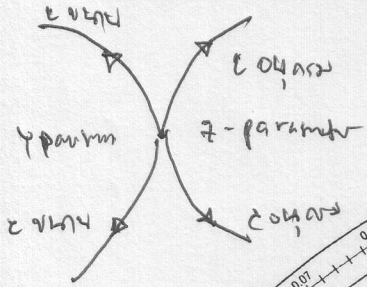
$$Z'_{in} = 0.25 - j0.375 \quad \Omega$$

3) In order to match Z'_L to Z_0 using Z'_{in} to use a series resistor
 or Admittance in Γ network from A to B to C

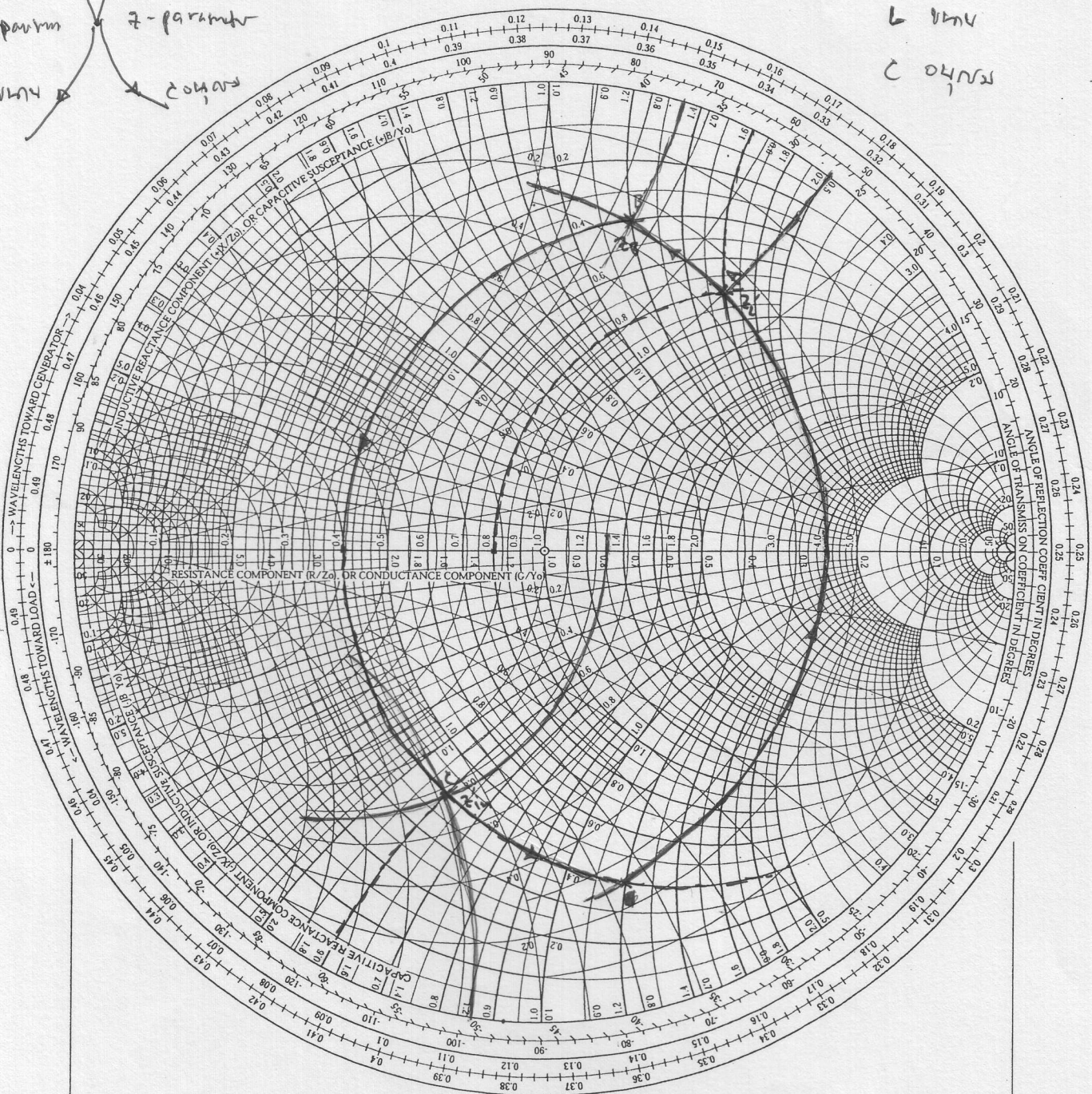
or A to B to C via L network
 B to C to A via C network

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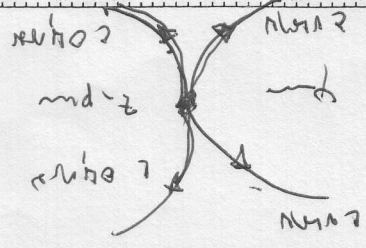
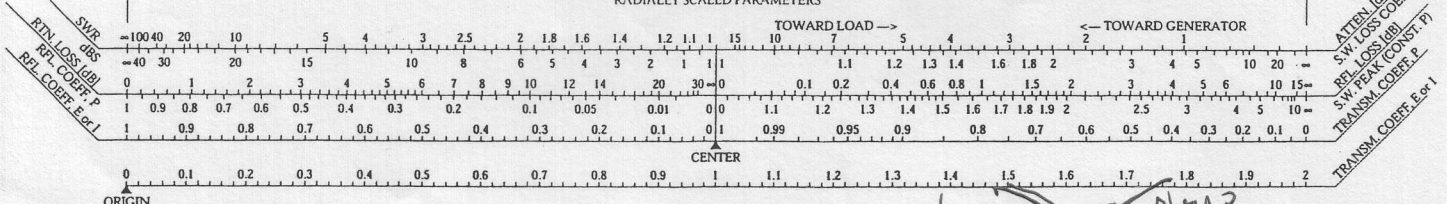
NORMALIZED IMPEDANCE AND ADMITTANCE COORDINATES



L 04/02
C 04/02



RADIALLY SCALED PARAMETERS



101

Часть B

$$Z_B = 0.4 + j1.2$$

$$Y'_B = \cancel{0.25} - j \cancel{0.95} \quad 0.95$$

Уч L vlyy

$$-jB_L = Y'_B - Y'_L = (0.25 - j\cancel{0.95}) - (0.25 - j0.5)$$

$$-jB_L = 0.25 - j0.95 - 0.25 + j0.5$$

$$-jB_L = -j0.25$$

$$B_L = \frac{Z_0}{\omega L} = \frac{Z_0}{2\pi f L} = 0.25$$

$$L = \frac{Z_0}{2\pi f 0.25} = \frac{50}{2\pi \times (360 \times 10^6) \times (0.25)}$$

$$L = 10.61 \mu H$$

Уч C 04vz.

$$-jX_C = Z_{iy} - Z_B = 0.4 - j0.6 - (0.4 + j1.2)$$

$$-jX_C = \cancel{0.4} - j0.6 - \cancel{0.4} - j1.2$$

$$-jX_C = -j1.8$$

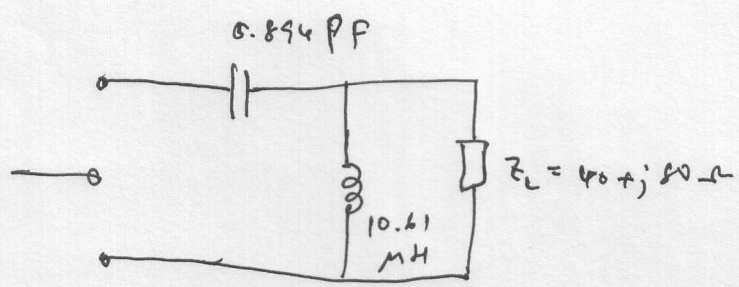
$$X_C = 1.8$$

$$X_C = \frac{1}{\omega C Z_0} = \frac{1}{2\pi f C Z_0} = 1.8$$

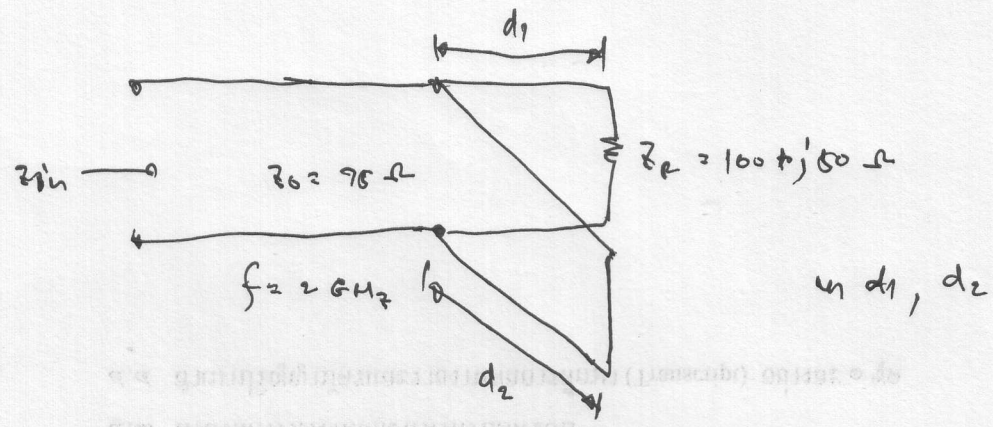
$$C = \frac{1}{2\pi f Z_0 (1.8)}$$

$$C = \frac{1}{2\pi \times (700 \times 10^6) \times (80) \times (1.8)}$$

$$C = 3.894 \text{ PF}$$



sol 8



sol 2

Step 1 $Z_r' = \frac{Z_L}{Z_0} = \frac{100 + j50}{75} = 1.333 + j0.666$

Step 2 in Z_r' plot solve smith chart on constant SWR

Step 3 in smith chart Γ_r constant SWR. 0.472λ
 $(0.5 - 0.472)$

Step 4 distance $d_1 = 0.068 \lambda + 0.15$

$d_1 = 0.218 \lambda$

$\lambda = \frac{v}{f} = \frac{3 \times 10^8}{2 \times 10^9} = 0.15 \text{ m} = 15 \text{ cm}$

$d_1 = 0.218 (0.15) = 0.0327 \text{ m}$

$d_1 = 3.27 \text{ cm}$

Step 5 in step 1 given Admittance value Y_0 solve

$Y_0 = \frac{Y_L}{Y_0} = 1 + j0.65$

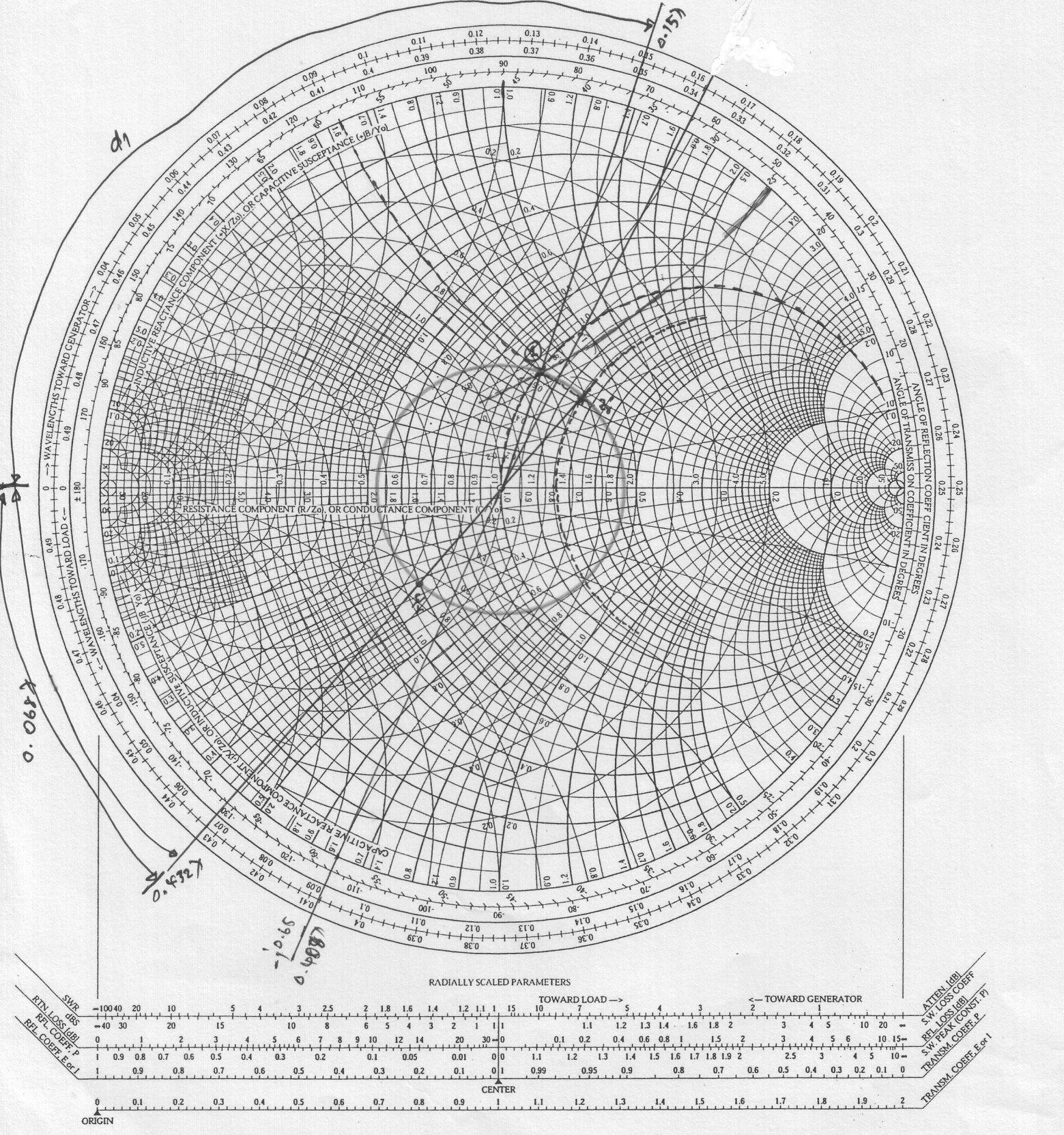
in smith chart solve for input admittance $= -j0.65$

Step 6 in smith chart solve for admittance 0.00Ω

on scale 0.00λ solve for admittance $-j0.65$

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NORMALIZED IMPEDANCE AND ADMITTANCE COORDINATES



$d_2 = 0.408 \text{ m}$

$d_2 = 0.408 (15 \text{ cm})$

$d_2 = 6.12 \text{ cm}$

$\therefore \text{a: } \left. \begin{array}{l} d_1 = 3.27 \text{ cm} \\ d_2 = 6.12 \text{ cm} \end{array} \right\}$